

TE Electrical Contractor Tococco

Serving the Florida Keys since 1989

**Date:** March 9, 2021

**Prepared by:** Caleb Mandile

**<u>Description:</u>** Historic Architecture Review Commission Application for a Grid-Tied Solar PV System for the Herr Residence: 898 United Street, Key West FL 33040.

**Preferred Layout:** 10x SunPower A410 Solar Panels resulting in 4,100 watts, with 3 mounted on the back flat roof, and 7 mounted as far back from the street as possible on the Southwest roof location. This system is designed to offset roughly 25% of the property's electricity consumption.



Image 1: Preferred Layout

**HARC Guidelines:** SALT Energy believes that the Preferred Layout shown above makes use of the most efficient roof surfaces while also accommodating the guidelines put in place by the Historic Architectural Review Commission to preserve the character of Key West. Each guideline is addressed in detail below.

- 1. HARC supports the introduction of new and emerging technology for renewable energy but will seek to achieve this by ensuring equipment is installed without permanent detriment to the historic fabric already established in the district and the least visual impact to buildings and streetscapes HARC's goal is high performance conservation with low public visibility. HARC recommends applicants exhaust all other ways of reducing the carbon footprint before putting forward applications for the installation of solar devices.
  The Herr Residence has already exhausted all other means to lower their carbon footprint. Since purchasing the house in January 2020, they have replaced the old A/C, ceiling fans, mini-fridge, and lightbulbs with new energy star models. They also installed a new ecobee thermostat to better regulate the temperature inside the home. Mr. and Mrs. Herr typically use their motor-scooters or bicycles as their primary source of transportation around the island. They do own one automobile that they rarely use except for long trips outside of Key West or for grocery runs.
- 2. Any proposal to install solar energy collectors shall be based on a hierarchy of preferred locations starting with roofing not visible from public streets, then locations within rear gardens or on pergolas and only if none of these are viable because of orientation or overshadowing will HARC consider schemes which involve collectors on roofing areas or other locations visible from public streets. Image 2.1 below is a reference of roof locations and how they will be referred to moving forward. The 4 solar water heater panels depicted in Image 2.1 are no longer present and were installed by the previous owner. Mr. and Mrs. Herr were not responsible for the solar water heaters and removed them since obtaining ownership in January 2020.



Image 2.1



Image 2.2: Preferred Layout, Layout 1

Image 2.2 above shows Layout 1, or the preferred layout that was decided upon using a hierarchy of roof surface preference based on maximizing efficiency while still meeting HARC guidelines. First, SE was prioritized as it has no visibility and is the most efficient location. When designing a layout, solar must allow a 36" perimeter around all rooftop equipment like A/C units for fire code, and a minimum of 10" between the edge of the array and any roof edges for wind-load requirements. Because of these limitations, only 3 panels could be mounted on SE. The remaining 7 panels could be mounted on SW or NE.

Both SW and NE are visible from United Street, but NE is obscured from view by the large tree in front of the house. However, according to criteria discussed during the pre-application meetings, trees are not considered when determining if a roof surface is visible or not. Therefore, SW and NE should be considered equally in terms of visibility from United Street.

SW is also visible from Margaret Street, as shown in Appendix 1 with 898 United circled in red. However, SALT would consider this visibility from Margaret street to be negligible due to past precedent with the solar water panels, which again Mr. and Mrs. Herr had no part in. These 4 solar water panels were never brought before HARC when they were initially installed by the previous owner and were never discovered by or reported to HARC during the duration they were on the roof. It was not until SALT provided an outdated satellite view layout of the new solar panel locations that the previous existence of these solar water panels was made known. SALT believes that the new 7 solar PV modules would have similar visibility. Unless a person had prior knowledge of their existence or saw them from a satellite view, the panels would not disrupt the view of the historic architectural landscape, even from Margaret Street. Therefore, the remaining 7 panels are mounted on SW according to Layout 1 for efficiency.

3. Any proposals that include collectors and/or related equipment and cabling visible from public streets will be required to show (by way of calculation of energy outputs) that it is not possible to achieve similar performance from equipment located away from public view.

The preferred layout shown again in Image 2.2 was created using a hierarchy of roof surface preference based on maximizing efficiency while still meeting the HARC guidelines. If the 7 panels on SW are still considered visible from the street, the following calculations are provided to demonstrate the loss in efficiency of moving any of these panels to NE, the only other available surface. A ratio known as the Kilowatt-Hour per Kilowatt (kWh/kWp) is used as the basis for the efficiency loss calculations. This ratio tells us the expected yearly kWh energy yield for each kW of solar installed on a particular roof surface. This value changes depending on the geographic location, tilt, and azimuth of the solar array. An azimuth greater than 90° (East) and less than 270° (West) is ideal for solar. SALT Energy has determined the values in Table 3.1 using Helioscope software

which accounts for these parameters.

Roof Surface	SE	SW	NE
Azimuth	145°	235°	55°
Tilt	5°	30°	30°
kWh/kWp	1,547.6	1,537.5	1281.4
Energy Loss	N/A	0.7%	17.3%

Table 3.1

This means that every watt of solar installed on NE will produce 16.6% less energy per year than the equivalent on SW. Since 70% of this system is located on SW, moving those 7 panels to NE would reduce the energy output of the entire system by 13%. This is why the preferred layout utilizes SW for the remaining 7 panels.

- Installations shall not exceed power generation greater than that reasonably needed for the property. All applications must contain calculations of power outputs and on energy retained.
   898 United utilized 27,485 kWh of electricity between November 8<sup>th</sup> 2019 and November 7<sup>th</sup> 2020 according to Keys Energy records shown in Appendix 2. Layout I Image 2.2, using the expected energy yield values shown in table 3.1 above, would be expected to produce about 6,400 kWh of electricity per year. This equates to an electricity use offset of about 25%.
- 5. Character defining features of existing buildings (i.e. roofline, chimneys, and dormers) shall not be damaged or obscured when introducing new roof or exterior wall-mounted energy conservation systems.
  The roofline of 898 United will not be affected by the addition of solar panels according to Layout I, Image 2.2. All panels will be installed a minimum of 10" from all roof edges to meet wind-load requirements.

- 6. All energy collection equipment shall be screened or hidden to the greatest possible while still achieving maximum function and effectiveness.

  Layout I maximizes the use of low visibility locations to screen or hide the panels while still prioritizing the more efficient surfaces over less efficient surfaces. The panels on SE will be hidden from view as SE is a rear facing roof section that is entirely hidden from street view. The panels on SW will be mounted as far away from the road as possible with the distance from the back edge of the array to the back edge of SW being 10". This leaves over 10 feet of space from the front of SW to the leading edge of the array.
- 7. On pitched roofs, solar collector arrays shall run parallel to the original roofline and shall not rise above the peak of the roof. On flat roofs, solar collector arrays shall be set back from the parapet edge or wall/roof conjunction and may be set at a slight pitch if not highly visible from public streets.

  All panels will be installed a minimum of 10" from the roof peak and any roof edges to meet wind-load requirements, therefore the panels will not rise above the peak of the roof. All panels will be installed parallel to the original roofline.
- 8. All energy collection equipment shall be considered part of the overall design of the structure. Color, shape and proportions of the solar collection array shall match the shape and proportions of the roof. Single installations on single-plane roofs are preferable to disjointed arrays or arrays on multiple roof planes. If more than one array is needed, it shall be limited to one panel section on each side of the structure if the arrays cannot be placed on a rear location. Scattered or disjointed arrays are not appropriate.
  The proportions and shapes of all arrays are designed to match the shape and proportions of the roof. No arrays will exceed the proportions of the roof they are installed on. All arrays will stay within the "shape" or boundary of the roof surface it is installed on. Layout I utilizes all available space on the rear location (SE) and based on visibility from the street, qualifies as a single installation on a single plane roof as described above with the remaining 7 panels mounted on SW.
- 9. All energy collection equipment shall not be mounted to project from walls or other parts of the building.No equipment will be mounted to project excessively from the walls of the building. No wall-mounted equipment will be visible from the street.

**Appendix 1:** Margaret Street Visibility



### **Appendix 2:** Keys Energy Records:

ACCOUNT_NO	OCCUPANT_CODE	BILLDATE	USAGE_BILLED	DEMAND_KW	ACCOUNT_NO2	OCCUPANT_CODE3	NAME	SERV_STREET_NO	SERV_STREET	SERV_UNIT
1024210	31	Nov 6, 2019 12:00:00 AM	1583		1024210	31	THOMAS JOSEPH HERR	89	8 UNITED ST	
1024210	31	Dec 6, 2019 12:00:00 AM	2085		1024210	31	THOMAS JOSEPH HERR	89	8 UNITED ST	
1024210	31	Jan 8, 2020 12:00:00 AM	1451		1024210	31	THOMAS JOSEPH HERR	89	8 UNITED ST	
1024210	31	Feb 6, 2020 12:00:00 AM	2358		1024210	31	THOMAS JOSEPH HERR	89	8 UNITED ST	
1024210	31	Mar 6, 2020 12:00:00 AM	3423		1024210	31	THOMAS JOSEPH HERR	89	8 UNITED ST	
1024210	31	Apr 9, 2020 12:00:00 AM	2991		1024210	31	THOMAS JOSEPH HERR	89	8 UNITED ST	
1024210	31	May 6, 2020 12:00:00 AM	2206		1024210	31	THOMAS JOSEPH HERR	89	8 UNITED ST	
1024210	31	Jun 8, 2020 12:00:00 AM	2428		1024210	31	THOMAS JOSEPH HERR	89	8 UNITED ST	
1024210	31	Jul 8, 2020 12:00:00 AM	2189		1024210	31	THOMAS JOSEPH HERR	89	8 UNITED ST	
1024210	31	Aug 6, 2020 12:00:00 AM	1718		1024210	31	THOMAS JOSEPH HERR	89	8 UNITED ST	
1024210	31	Sep 9, 2020 12:00:00 AM	1783		1024210	31	THOMAS JOSEPH HERR	89	8 UNITED ST	
1024210	31	Oct 7, 2020 12:00:00 AM	2279		1024210	31	THOMAS JOSEPH HERR	89	8 UNITED ST	
1024210	31	Nov 6, 2020 12:00:00 AM	2574		1024210	31	THOMAS JOSEPH HERR	89	8 UNITED ST	

### **CONSTRUCTION PLANS FOR** SOLAR PV SYSTEM HERR RESIDENCE



898 United Street Site Location:

Key West FL 33040

Salt Service Inc. Solar Installer:

2992 Overseas Highway

Marathon, FL 33050 (305) 289-1150

FL SOLAR CONTRACTOR LICENSE: CVC56734

CUSTOMER: SHEET #: SYSTEM: TITLE 898 United Street, Key West FL 33040 10 x Sunpower A410's - 4100 Wp Traci Herr SCO 027-100 **Herr Site** PROJECT #: DATE: SALT ENERGY 2992 Overseas Highway, Marathon, FL SALT Service, Inc.

(305) 289-1150

SCO 027 2/23/21

1 3 7

Structural Calculations - PV racking & attachment Florida Building Code 2014, ASCE 7-10, CPP Wind Tunnel Test Report 9790 (12/29/16)

### Dimensions

Roof height:	30 ft	
Roof slope:	18.50 des	TO BOTH
PV module long dimension:	5.12 ft	NO SENS
PV module short dimension:	3.43 ft	1
Rail tributary width:	2.56 ft	The same
Gable End Width, W =	40.00 ft	*
Ridge Length, L =	60.00 ft	STATE O
Dead Loads		S
Rail:	0.56 lb/ft	ALL CHARLES
	0.2 psf	
Module:	46 lb	
	2.6 psf	
Total:	2.8 psf	
	7.3 lb/ft along rail	
Load normal to PV surface:	6.88 lb/ft along rail	
Load parallel to PV surface:	2.30 lb/ft along rail	
Snow Loads		
Ground snow load ne:	0 -6 -6 -6 -6 -6 -6 -6 -6 -6 -6 -6 -6 -6	



Snow Loads	
Ground snow load pg:	0 psf (ASCE 7 Figure 7-1 and Table 7-1)
Ct	1.20 (ASCE 7 Table 7-3)
Ce:	0.90 (ASCE 7 Table 7-2)
IS:	1 (ASCE 7 Table 1.5-2)
S.	0.94 (ASCE 7 Figure 7-2)
The sand sand sand sand sand sand sand sand	

0.00 lb/ft along rail	oad parallel to PV surface:
0.00 lb/ft along rail	Load normal to PV surface:
0.00 psf (ASCE 7 Equation 7.4-1)	slaped roof snow load ps:
0.00 psf (ASCE 7 Equation 7.3-1)	Hat root snow load pr:
0.94 (ASCE 7 Figure 7-2)	
T (UNCT ) (BOIC T'D'S)	,

Wind Loads	
Wind Speed V:	180 mph (ASCE 7 Figure 26.5-1)
Exposure:	D (ASCE 7 Section 26.7.3)
K2:	1.16 (ASCE 7 Table 30.3-1)
(Note: More conservative than 159	(Note: More conservative than 15% increase over Exp C as recommended in wind tunnel report, so ok.)
Kzt:	1.00 (ASCE 7 Section 26.8.2)
Kd:	0.85 (ASCE 7 Table 26,6-1)
0 = 0 00256K2K2K4KdVA2 =	0104 6/1007

	1.00 (ASCE 7 Section 26.8)	ore conservative than 15% increase over Exp C as recommended in w	_	Kzt: Kd: q = 0.00256KzKztKdV^2 = GCn = VE =
Kz: 1.16 (ASCE 7 Table 30.3-1)  (Note: More conservative than 15% increase over Exp C as recommended in wind tunnel repr	1.16 (ASCE 7 Table 30.3-1)		1.16 (ASCE 7 Table 30.3 the than 15% increase over Exp C as recommended in	ore conservative th
D (ASCE 7 Section 26.7.3) 1.16 (ASCE 7 Section 26.7.3) 1.16 (ASCE 7 Table 30.3-1) 1.6 (ASCE 7 Table 30.3-1) 1.0 (ASCE 7 Section 26.8.1)	D (ASCE 7 Section 26.7 1.16 (ASCE 7 Table 30.3-1		D (ASCE 7 Section 26 1.16 (ASCE 7 Table 30.3 tive than 15% increase over Exp G as recommended in	Exposure: Kz: (Note: More conservative th

Maximum Demands on Roll/Connections
Worst Case Upilit
Worst Case Downward
Worst Case Seismic Demand
Worst Case Shear for Pulift Cases
Worst Case Shear for Downward Cases
Worst Case Shear for Downward Cases
Worst Case Shear for Seismic Cases

-187.31 113.07 7.92 2.07 3.22 7.14

P P P P

	4.38 lb/ft along rail	Load parallel to PV surface: +/-
	-0.34 lb/ft along rail	Load normal to PV surface: +/-
	1.06 lb/ft along rail	Vertical load Ev = 0.2*Sds*Wt =
	4.26 lb/ft along rail	Horizontal load Eh:
	0.42 psf (ASCE 7 Equation 12.4-4)	FV = 0.2*Sds*Wt =
	1.66 psf (ASCE 7 Section 13.3.1)	
V <sub>stach</sub> = w*L		Fp = (0.4*ap*Sds*Wt*(1 + 2*zh)) / (Rp/lp) =
	1.00 (ASCE 7 Section 13.3.1)	z/h:
P = w*L	1.5 (ASCE 7 Table 13.6-1)	RD:
	1 (ASCE 7 Table 13.6-1)	ap:
I = W*L =	1.00 (ASCE 7 Section 13.1.3)	Ď:
Attacha	0.733333 (ASCE 7 Equation 11.4-3)	Sds:
D/Ctown =	1.1 (ASCE 7 Equation 11.4-1)	Sms:
Praticul down	1.1 (ASCE 7 Table 11.4-1 -Site Class D)	Fax
Managhadawa -	D (ASCE 7 Section 11.4.2 - Assumed)	Site Class:
\$	1 g (ASCE 7 Figure 22-1)	Ss:
D/Cup =		Seismic Loads
Malaway =	104.81 lb/ft along rail	Load normal to PV surface Up =
Check Stre	-193.50 lb/ft along rail	Load normal to PV surface Up =
Max allowa	-75.64 psf (CPP Report Equation 8) 40.97 psf (ASCE 7 Downforce)	Pressure Up = Pressure Down =

x allowable cantileve	attachme	ximum Allawable Spacing
tilever	igned attachment spacing	le Spacing

1.00 (CPP Report Figure 3-5)

		18*w*L² =	able cantilever	ttachment spacing	Allowable Spacings
0.68 OK	-548	-375	14.00	48.00	
OK	-548 lb-ft	lb-ft	5	5	

Pown = W*L =	SCE 7 Table 13.6-1)
	SCE 7 Table 13.6-1)
1 = W*L =	SCE 7 Section 13.1.3)
Attachment L	SCE 7 Equation 11.4-3)
LIMBO COMPL	SCE 7 Equation 11.4-1)
D/C =	SCE 7 Table 11.4-1 -Site Class D)
N	SCE 7 Section 11.4.2 - Assumed)
× = 1	(ASCE 7 Figure 22-1)
D/Cup =	

Load Combinations - Ib/ft along rail			
1.4D	9.6		٧
1.2D+1.6S+0.5W (All Zones)	60.7	VN	
1.2D+0.5S+1.0W (All Zones)	113.1	oov	
1.2D+1.0E+0.2S	7.9	c	MA
0.9D+1.0W	-187.3	UP	NOR
1.4D	3.2		
1.2D+1.6S	2.8	N	EL
1.2D+0.5S	2.8	w	ALL
1.2D+1.0E+0.2S	7.1	DC	AR
06'0	21		100 min 100

allowab	ned att	mum Al
ax allowable cantilever	signed attachment spacin	eximum Allowable Spacing

D/Cup =	Malance =	Mmacuo = 1/8*W*L' =	Check Strength of Rail	Max allowable cantilever	Designed attachment spacing	Maximum Allowable Spacings

	- J.M.8/1

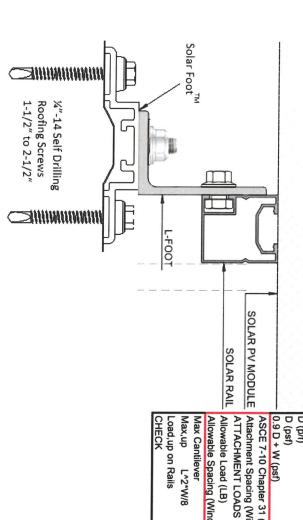
		W"L" =	
0.39 OK	580 lb-ft	226	
OK	lb-ft	Ib-ft	- Charles

w*L =	nent Loads	

٦,	-	e
29 lb	452 lb	-749 lb

ппсе	Wind Load Calulations
SHEET #:	SCO 027-200
SYSTEM:	10 x Sunpower A410's - 4100 Wp
CUSTOMER:	Traci Herr
898 U	898 United Street, Key West FL 33040
PROJECT #:	SCO 027
DATE:	2/23/21

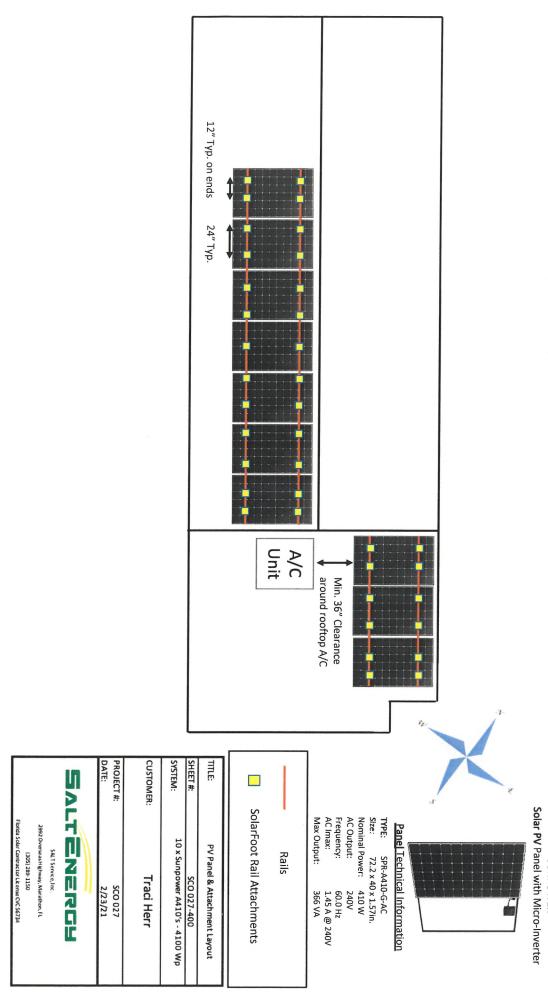




				П	I	]									-
	L-FOOT						*								
						SOLAR RAII	SOLAR PV MODULE	!							
CHECK	Load,up on Rails	Max,up L^2*W/8	Max Cantilever	Allowable Spacing (Wind Tunnel)	Allowable Load (LB)	ATTACHMENT LOADS	Attachment Spacing (Wind Tunnel):	ASCE 7-10 Chapter 31 (Wind Tunnel Procedure)	0.9 D + W (psf)	D (psf)	D (p/f)	W (LB/ft on Rail)	L (1/2 of 1 Panel in portrait)	Pressure UP Wind Tunnel)	WIND LOAD CALCS
0.207619 OK	-548 ft-lb	-113.8 ft-lb	14	29.4	558 SOLARFOOT	-455.101 lb	24 in.	el Procedure)	-219.969 WORST CASE UPLIFT	2.8	8.423333	-227.55	3.008333 10.03	-75.64 Trib Area	180D
a = 4.00	Max Allowed Load on rail is 1096 lb	Max Attachment Spacing C&C ZONE 3 (in)	Max Attachment Spacing C&C ZONE 2 (in)	Max Attachment Spacing C&C ZONE 1 (in)	Sola	MAXIMUM SPACING BASE	S-5 SOLARFOOT ANCHOR	ASCE 7-10 Chapter 30 (Components and Cladding)	IPLIFT	Racking Weight (lbs)	72.2	Panel L (in)	6.02	Panel L (ft)	Small Frame Panel A-Series
	96 lb	20NE 3 (in) 16.6	ZONE 2 (in) 24.6	ZONE 1 (in) 42.8	Solarfoot with 4 x 1/4" Screws	MAXIMUM SPACING BASED ON 2X SAFETY FACTOR	S-5 SOLARFOOT ANCHOR in MINIMUM 19/32" PLWOOD	onents and Cladding)		56.16	40	Panel W (in)	3.33	Panel W(ft)	

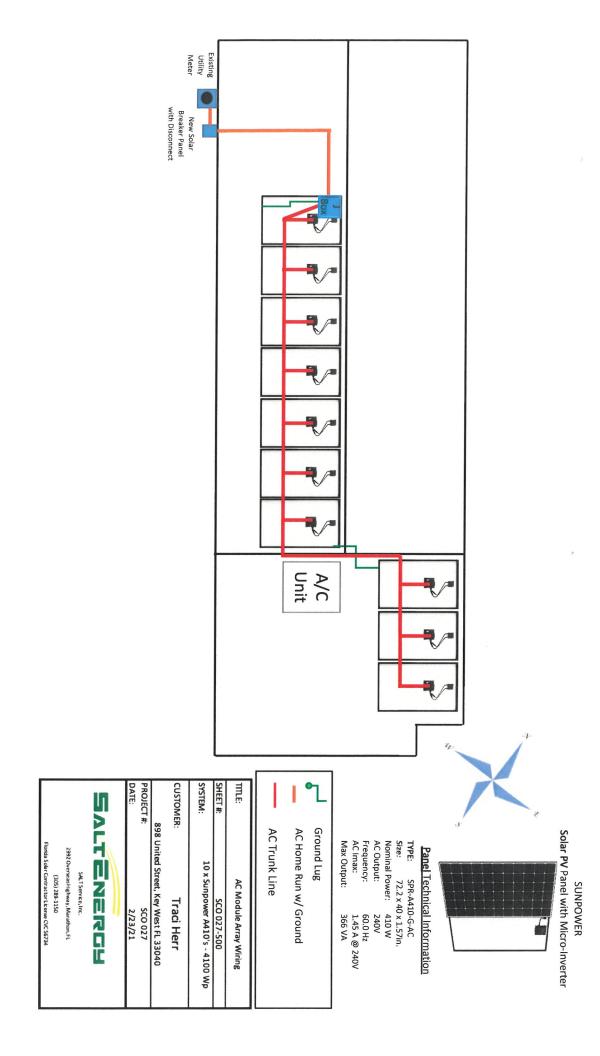
<b>Load Test Results</b>	Results		
Name	Product Information	Panel Information	Peak Load (lbf)
Test 1	SolarFoot (4) 0.25 14 Self Drilling Screw 1-1/2" to 2-1/2"	19/32" Plywood	915.608
Test 2	SolarFoot (4) 0.25 14 Self Drilling Screw 1-1/2" to 2-1/2"	19/32" Plywood	1209.744
Test 3	SolarFoot (4) 0.25 14 Self Drilling Screw 1-1/2" to 2-1/2"	19/32" Plywood	1038.427
Test 4	SolarFoot (4) 0.25 14 Self Drilling Screw 1-1/2" to 2-1/2"	19/32" Plywood	1300.195
		Mean	1115.993
		Standard Deviaton	172.134
		Allowable load (Safety factor of 2)	557.9965

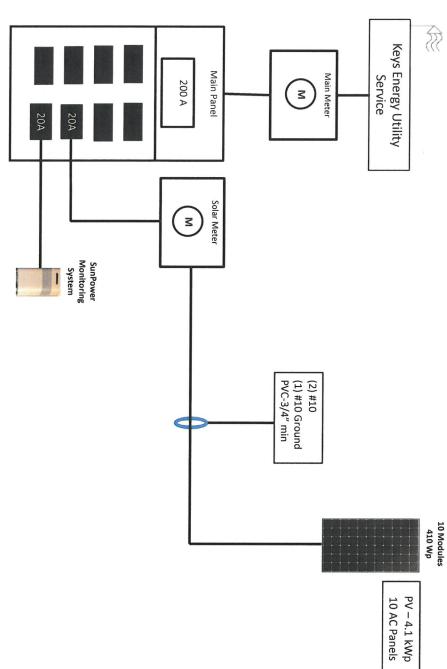
шпе	Attachment Details
SHEET #:	SCO 027-300
SYSTEM:	10 x Sunpower A410's - 4100 Wp
CUSTOMER:	Traci Herr
N 868	898 United Street, Key West FL 33040
PROJECT #:	SCO 027
DATE:	2/23/21
SAL	
	SALT Service, Inc.
	2992 Overseas Highway, Marathon, FL
	(305) 289-1150
F	Florida Solar Contractor License CVC 56734



SUNPOWER
Solar PV Panel with Micro-Inverter

1 .1. w





i ab m



THIS SERVICE METER
IS ALSO SERVED BY A
PHOTOVOLTAIC SYSTEM

**∠** WARNING

**ELECTRIC SHOCK HAZARD** 

DO NOT TOUCH TERMINALS
TERMINALS ON BOTH THE LINE AND
LOAD SIDES MAY BE ENERGIZED IN THE OPEN POSITION

### PHOTOVOLTAIC SYSTEM DISCONNECT

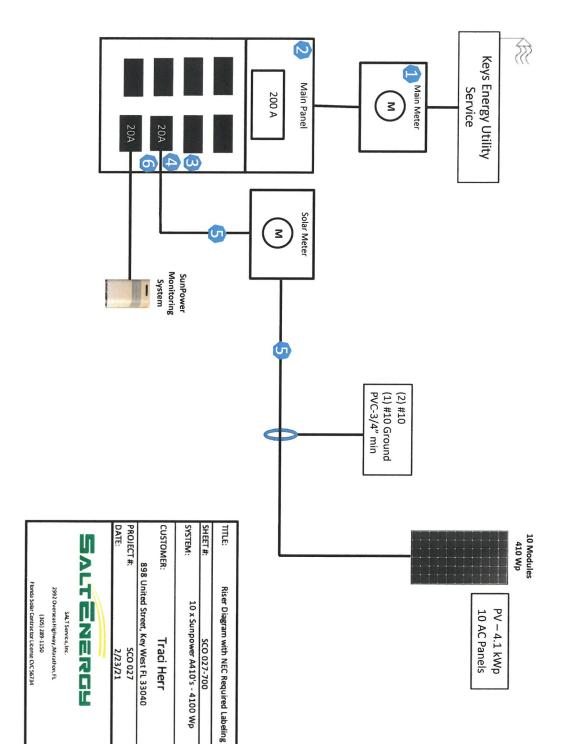
OPERATING VOLTAGE **OPERATING CURRENT** 240 VOLTS 14.5 A

\*\* WARNING A

SOLAR ELECTRIC BREAKER IS BACKFED

PHOTOVOLTAIC POWER SOURCE **NWARNING** 

SOLAR BREAKER





# SUNPOWER\*



Bu't spec' cally for use with the SunPower Equinox<sup>iii</sup> system, the only fully ntegrated solution designed, engineered, and warranted by one manufacturer



### Highest Power Density Available.

SunPower's new Maxeon" Gen 5 ce. 's 65% larger than prior generations, delivering the most powerful cell and in ghest-efficiency module in residential solar. The result is ava able so ar. nore power per square meter than any commercially



And Better. Fundamentally Different.



## Highest Lifetime Energy and Savings.

3

Designed to deliver 60% more energy over 25 years in real-world conditions. Ike partial shade and high temperatures.



SunPower® Maxeon® Technology

Most powerful cell in rome solar 
Deliver's unmatched reliability

Patented Sulid metal foundation prevents
breakage and corresion



### Best Reliability. Best Warranty.

**(0)** 

with the industry's best 25-year Combined Power and Product Warranty, including the highest Power Warranty With more than 25 m ion modules deployed around the world. SunPower technology is proven to last. That's why we stand behind our module and microinverter



# A-Series: A420 | A415 | A410 | A400 | A390 SunPower® Residential AC Module

Inverter Model: SPWR-A4 (Enphase IQ 7AS)	@240 VAC
Person the Bayer	WA 900
Max (curintarius Outside Brown)	VA 6:1
Non-Jest Vollage / Barage (V)	2427.211.224
She Company Outs, Flurency)	70.
"Augus" - act 20 AC (pitch at a trans-	( ) 4
s DAME of the District of	76076
Non-Friduerics	ALE
betarger forcus of Recy.	240345
At Shart Circust De Steam 11 Over 14 years	ЬЗАхия
Opervolute as ACPOS	

odine (Thioristy 32 LES 200)	000 Provide (Priorin) W   622   435   400   400   250	ARTHUR ACTIONAL WINDS AC MODERN ADMONIA	DC Power Data
20.9	250	3400 CAC	

	Tested Operating Conditions
Onerating Tento.	Castra of 340t-14481 to 0.440th-
May Amount to up.	(54t) (54t)
Max less cope	Wister (87 ps), grounds, grif Agyar ps), X Sinow 187 ps), grounds, grif Agyar ps), X
Desgradad	What 62's at Jabba Pu, 305 kg/m2 sack Show, 125 ast 6000 Pu, 611 kg/m2 trons
Inductives storee	Court 25 minut distinction may at 52 minut 23 minut
The second second second second	

Solar ciglis	Go Monocystal in Maxeon Gen 5
F00054400	Hgt furtsinske tempines gaskwith until deconociones
Environmenta Rating	0.0000 1040
Franc	Care mandarpaszed opeszákká rango
West	46.5 58.02.2 kg)
Resonancian Vax	

ofer PV Durability Initiative for Solar Modules: Part 3." PVTech Power mpeau. Z. et al. "Sun Power Module Degradation Rate." Sun Power white

CB.





SUNPOWER

when the state of the state of

60% lighter than prior SunPower MIs Engineered and calibrated by SunPower for SunPower AC modules

actory-integrated Microinverter (MI)



### Simple and Fast Installation

- assembled mid and end clamps
- hid camp width facilitates consistent, even ating mid clamp for easy placement

### Flexible Design

- ils enable easy obstacle managemen

### Customer-Preferred Aesthetics

- in cass system aesthetics nodule and #1 mounting aesthetics
- emium, law-profile design
- Hidden mid clamps and capped. Bush

### Part of Superior System

- It for use with SunPower DC and AC module:
- Riniclass system reliability and aesthetics
- aunal rooftop transition flashing, rail-ounted J-box, and wire management rail clips





### Elegant Simplicity

system-level approach amplifies the aesthetic and installation benefits - for homeowners and for installers engineered to pair with SunPower modules. The resulting The invisiMount product was specifically envisioned and addresses residential sloped roots and combines faster rail based mounting system. The invisiMount system SunPower\* InvisiMount\* is a SunPower-designed aliation time, design flexibility, and superior aesthetics





SUNPOWER

















	ings.	salient foliates, n8	MA	om Lineau \$5364 185 (0.6342)	9.43	and series
E	75 s (2 e oz)	106.5 g (8.75 oz)	LOUIT.	188 (0.52.02)	820 g/m (9 oz/ff)	6303/m (202/II)
		40.301.118	Contract sensor	ALL AND ALL		
	CS DALLT	Sommon .	A CAPITAL MANAGEMENT PROPERTY.	The same of the sa		TOTAL DESIGNATION OF

entry series and any
A. A. S.

103	IC 000.	340 14 E	HIC 98-	280 PHE	Selfs of It
Refer to roof attactment meawweematcher seets		Rolls at action marchage with a			A SECURITION OF THE PARTY OF

e de la company de la comp La company de la company d

SUNPOWER.

# 2.1 Fire Classification

- The maximum distance between the roof deck and the bottom of the module frame is 3" (7.6 cm).
- In order to maintain the system classification, this assembly must be mounted over a fire resistant roof covering for the application.
- The system achieves a Class A fire rating when installed with modules having a Type 2 fire classification; or for modules specifically fire tested with the invisiMount system.
- The system achieves a Class A fire rating when installed in the manner specified in these instructions.
- The system was evaluated for use on roofs having a pitch ≥ 2\*floot (greater than or equal to 2:12).

# 3.0 System Ground Path

The InvisiMount system features:

- Integrated module-to-rail as well as adjacent-module bonding (achieved through the mid clamp and end clamp).
- Integrated rail-to-rail bonding (achieved through the self-drilling splice screws and the splice).
- System bonding achieved through the equipment ground conductor (EGC).

For arrays where the installer chooses to use row-to-row (R2R) grounding clips (refer to Section 5.6.1) instead of additional ground lugs and copper wife, system bonding is achieved through the R2R clips.

without the R2R grounding clip: The following two diagrams illustrate the key grounding and bonding aspects of the InvisiMount system with and

- the system ground path
- each component
- the applicable NEC and UL references

- each bonding point

# 5.5 Attach Ground Wire

For arrays with two or more rows, in order to achieve row-to-row grounding, you must install

- one ground wire, one ground lug assembly, and an R2R grounding clip (Fig. 10 and Section 5.6.1) Note: An R2R grounding clip is required between each row pair—e.g. a three-row array
- two ground wires and two ground lug

would require two R2R clips.

If your array has a standalone module (refer to Section 5.7), you must install a ground lug assembly on one of its rails as wel. assemblies (Fig. 11)

Important! Ensure that you install the system such that the copper ground wire will never contact any aluminum! (Refer to Fig. 16.)

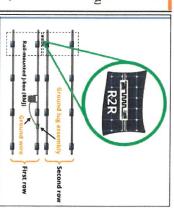


Fig. 10



Fig. 11

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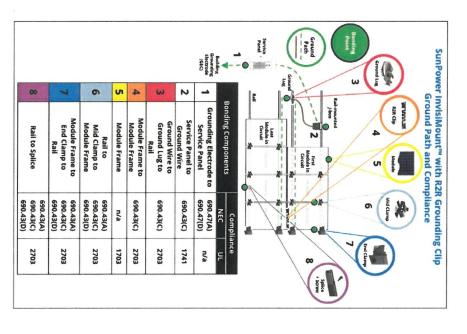
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#508988 Revik

Ground Path Service Panel Ground Lug U w 9 4 N **Bonding Components** Grounding Electrode to Service Panel Rail-mounted J-box Rail to
Mid Clamp to
Module Frame
Module Frame to
End Clamp to
Rail Last Module in Circuit Ground Wire to Ground Lug to Service Panel to Ground Wire **Module Frame** Rail to Splice Rail 690.47(A) 690.47(D) 690.43(A) 690.43(C) 690.43(D) 690.43(A) 690.43(C) 690.43(D) 690.43(A) 690.43(C) 690.43(D) 690.43(C) 690.43(C) n/a NEC Compliance 0 2703 2703 1741 2703 2703 1703 n/a 드 Splice + Screw

SunPower InvisiMount™ Ground Path and Compliance

Module



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